

Modulation Index Boosting (MiBo) and Enhanced PDV Sensitivity for Unconventionally High-Velocity Objects

David Borlaug,^{1,2} Bill Seng,² Crystal Glen,² and Bahram Jalali¹

¹University of California, Los Angeles

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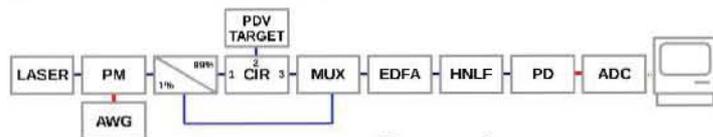
Tuesday, June 7, 2016, 2:20 PM - 2:40 PM
Photon Doppler Velocimetry Workshop, 2016
The Bankhead Theater -- Livermore, California

- Modulation Index Boosting (MiBo)
 - Concept, Principles, Simulations, Experiments, Prototype
- PDV at Sandia's Z-Machine, one example from 2013
- General PDV Model & Waveform Synthesis
- MiBo & PDV
- Future Enhancements: MiBo + Time-Stretch
- Summary / Discussion

Photon Doppler Velocimetry

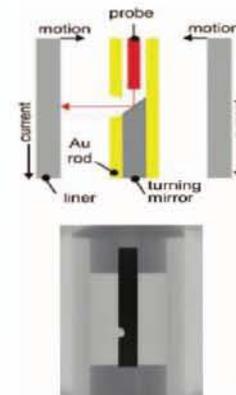
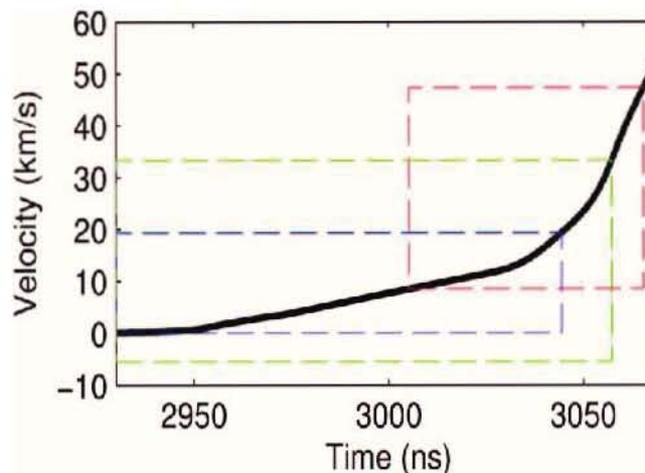
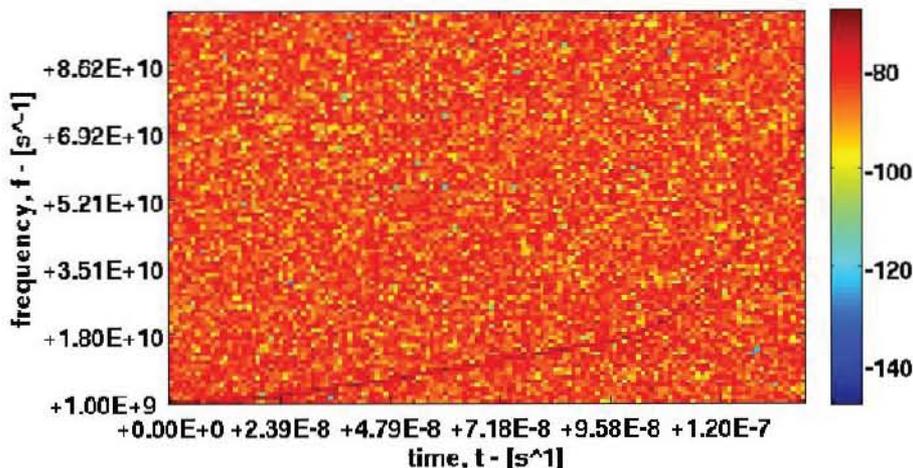


- Photon Doppler Velocimetry (PDV), developed by Sandia, utilizes Doppler velocimetry to track unconventionally high-velocity objects.
- PDV waveforms contain broadband 1-70 GHz content.
- Simulation show MiBo improves PDV detection sensitivity by 10 dB in general, and by 20 dB for signals beyond 40 GHz.
- Jalali-Lab's Time-Stretch Technology already deployed at DoE facility



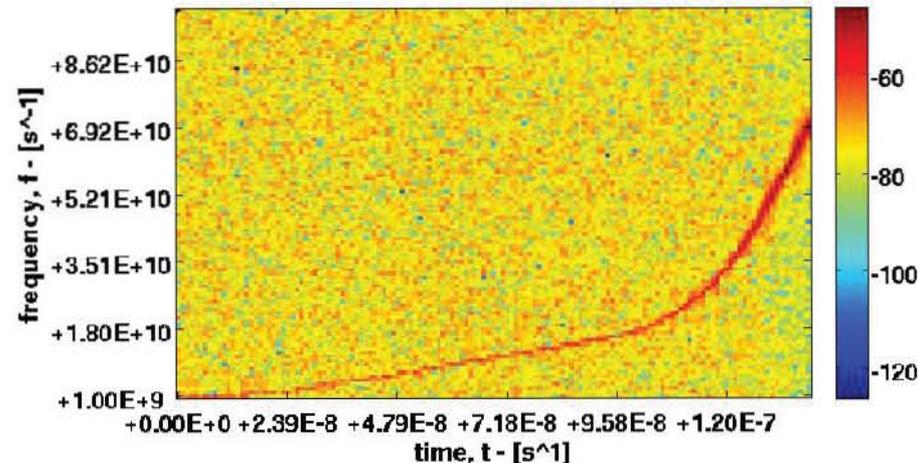
Conventional

power, P - [dBm]



MiBo

power, P - [dBm]

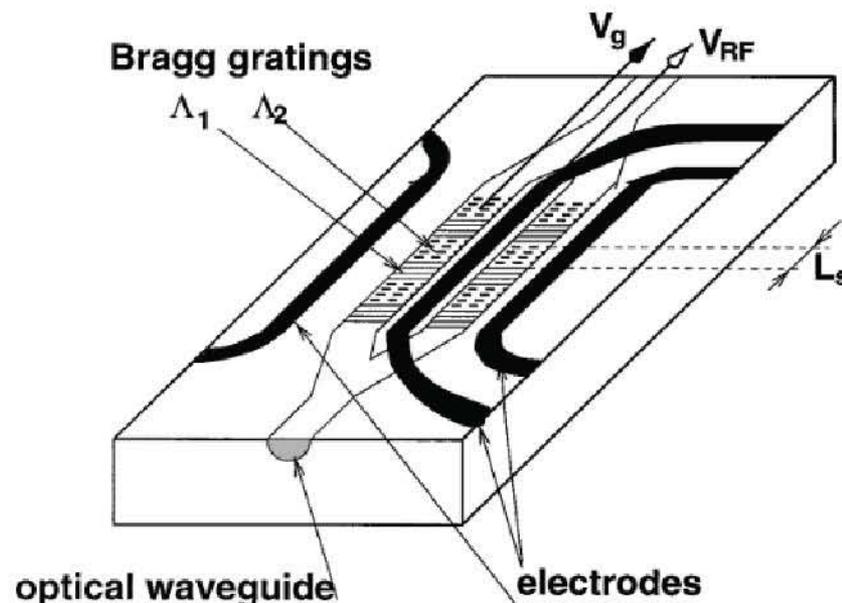


- **Velocity matching**

- **High r_{33} material**

Lithium niobate (LiNbO₃), $d_{33} = 30.9$ pm/V

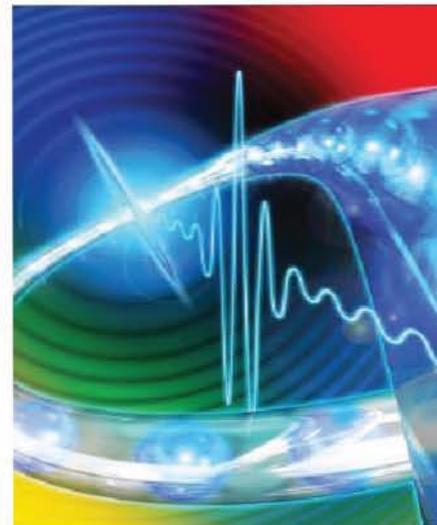
- **Resonant modulators**



- **Distributed RF amplification along the waveguide**

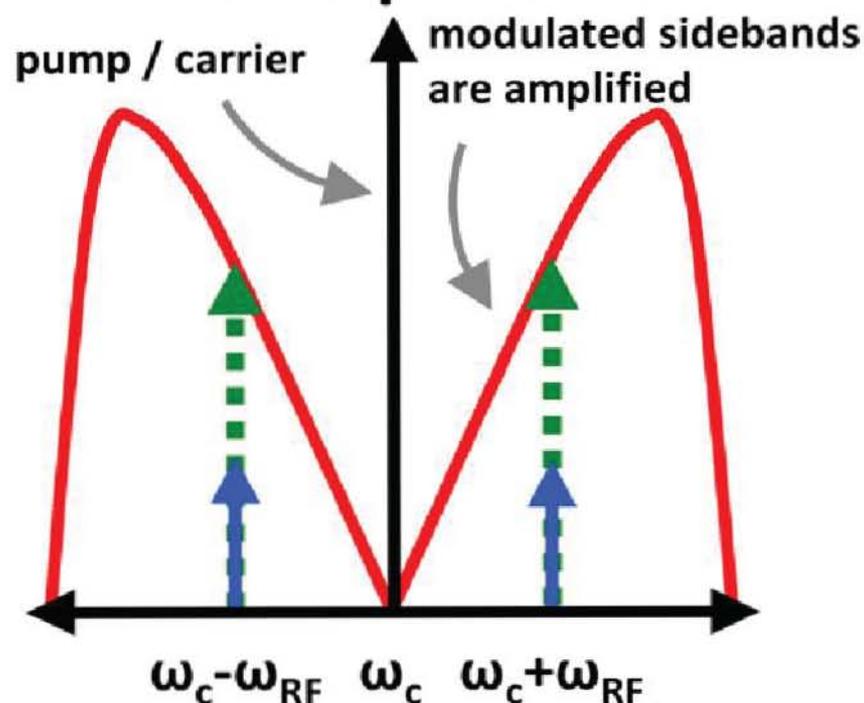
Are there other, previously unexplored approaches for Vpi reduction?

- Responsible for spontaneous pattern formation
- Sand ripples, cloud formations, water waves, coupled pendula, queues
- Optical rogue waves
Jalali-LAB, 2007
- Solitons & supercontinua
- Amplifies Sideband-only
(at the expense of the carrier)



MiBo exhibits high-pass frequency amplification, $g(\omega)$. Modulated sidebands are amplified at the expense of the pump/carrier to increase modulation depth and lower V_{π} .

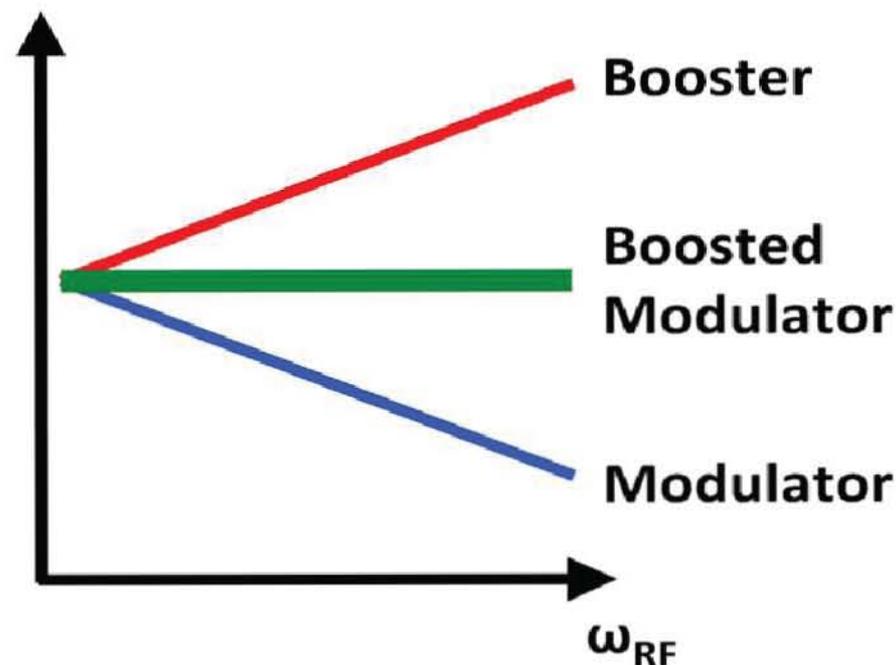
Gain Spectrum



$$g(\omega) = |\beta_2 \omega| \left[\left(\frac{4 \gamma P}{|\beta_2|} \right) - \omega^2 \right]^{1/2}$$

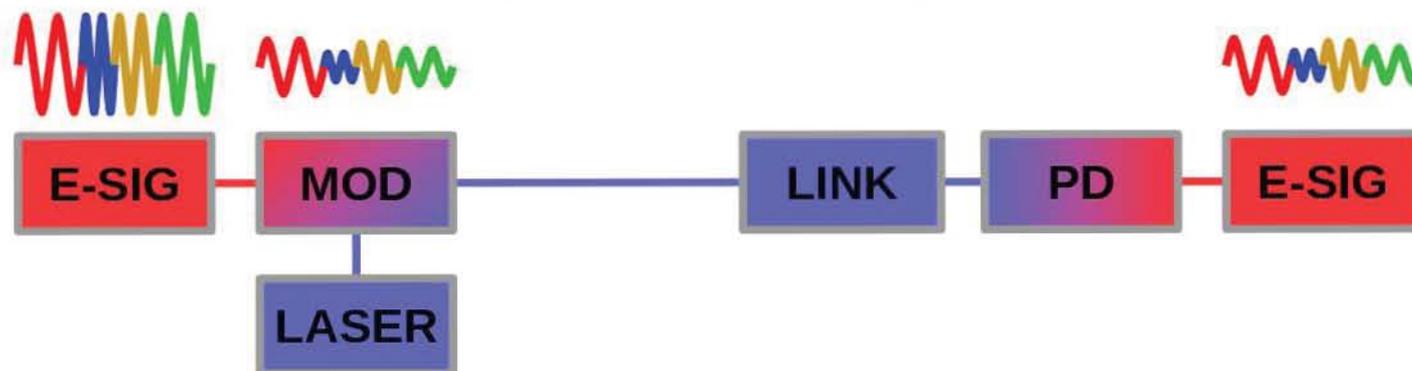
$$\Omega_c = 4 \gamma P / |\beta_2| \quad V_{\pi, \text{eff}}(\omega) = V_{\pi}(\omega) / \sqrt{G_{MI}(\omega)}$$

Modulation Depth

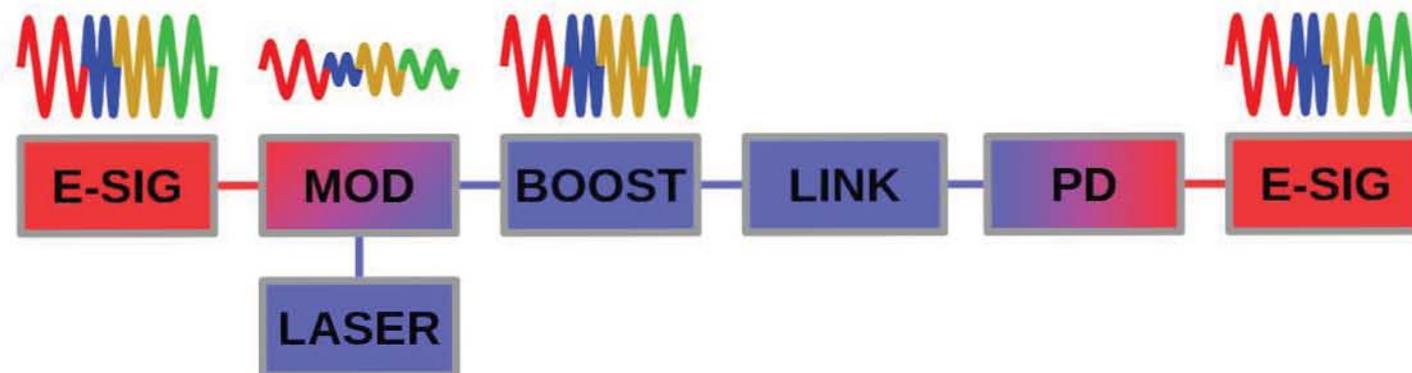


Boosted Modulator

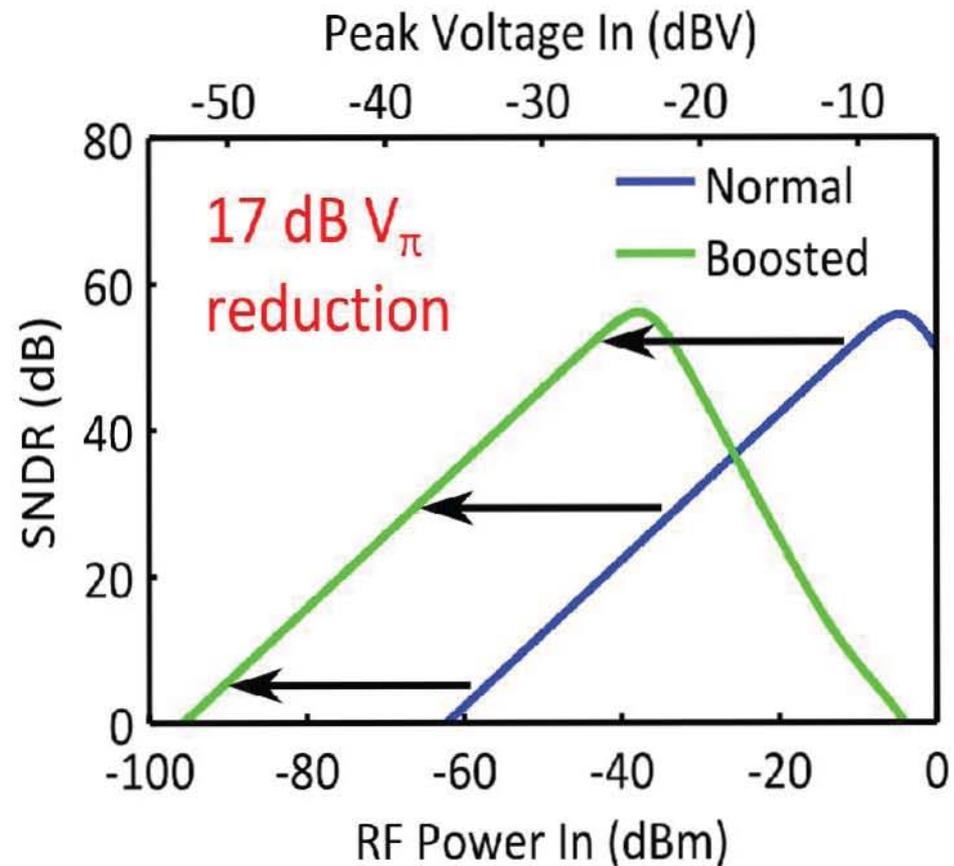
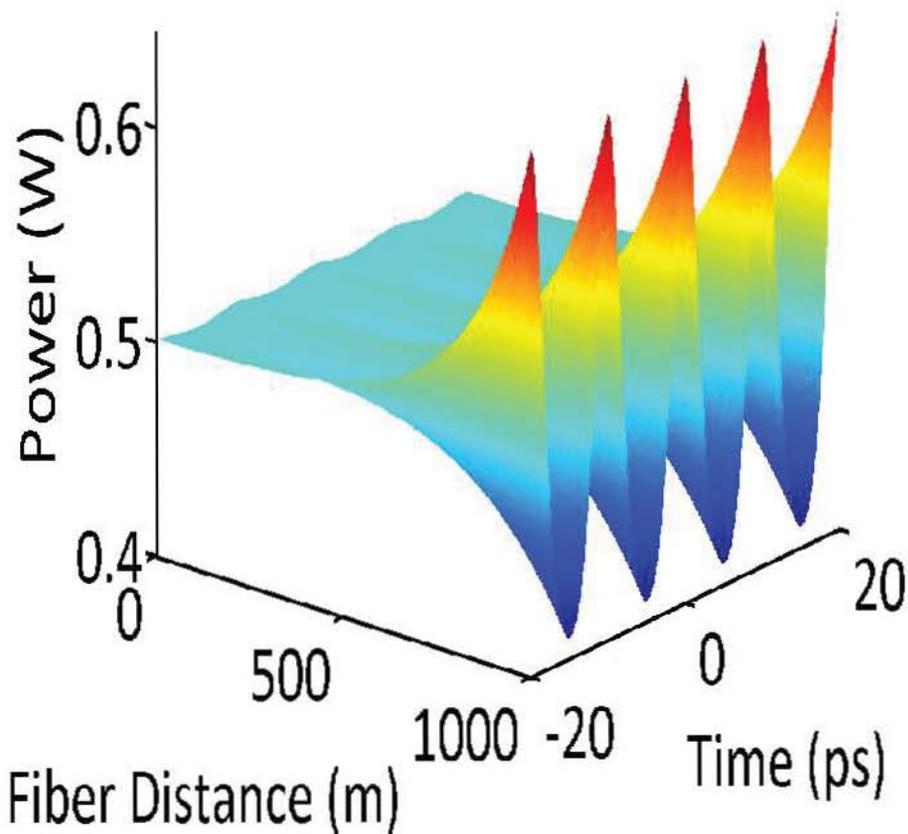
Conventional



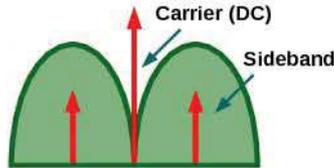
MiBo



Modulation Index Booster (MiBo)



$$SNR \propto P_{RF, out} \propto \frac{1}{V_{\pi, eff}^2}$$

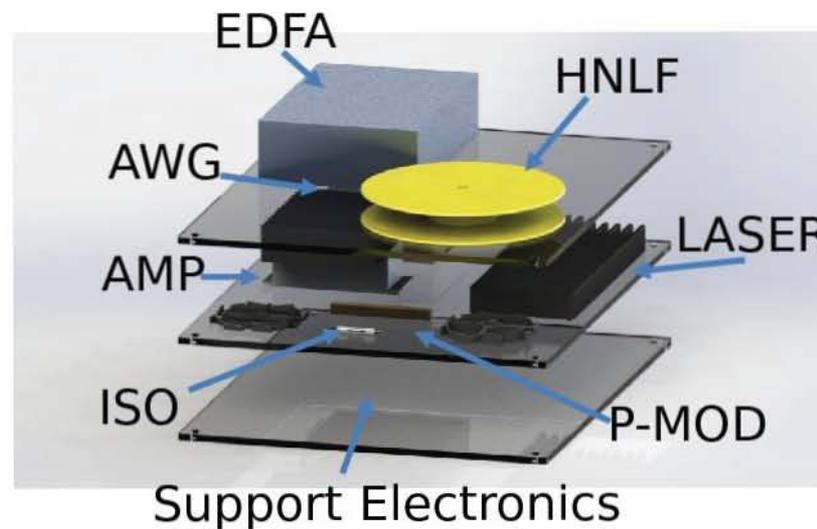
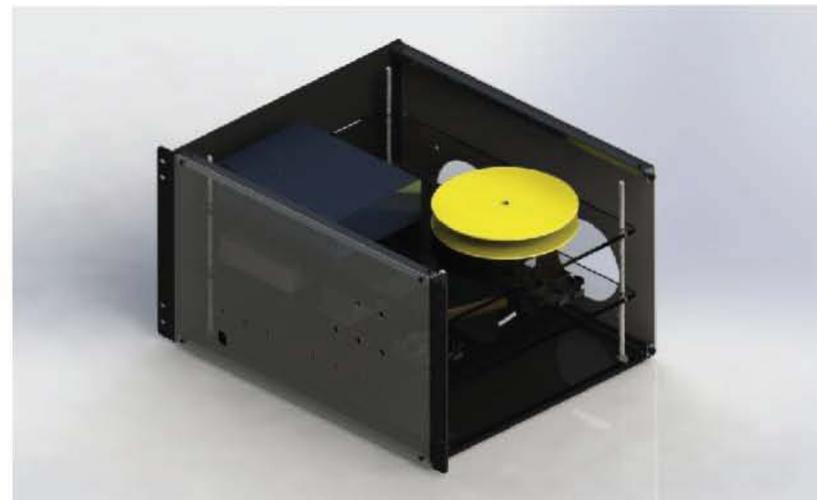
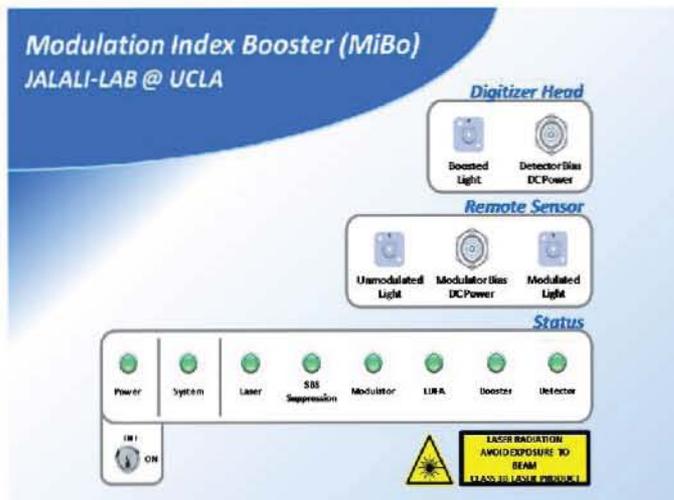


| | Carrier Filtering vs MiBo | |
|--------------------------------|---|------------------------------------|
| | Carrier Filtering | MiBo |
| Sideband Response | Net Loss: Passive Filter Insertion Loss | Net Gain: 15 dB @ 50 GHz |
| Carrier Response | Strongly Attenuated | Negligible Propagation Attenuation |
| Sideband:Carrier Specificity | Strong | Strong |
| Active Filter Tuning & Locking | Yes: Required | No: Self-Aligned |
| Temperature Drift | Yes | No |

| | EDFA vs MiBo | |
|--------------------------------|--------------------|------------------------------------|
| | EDFA | MiBo |
| Sideband Response | Strongly Amplified | Net Gain: 15 dB @ 50 GHz |
| Carrier Response | Strongly Amplified | Negligible Propagation Attenuation |
| Sideband:Carrier Specificity | Poor | Strong |
| Active Filter Tuning & Locking | No: Self-Aligned | No: Self-Aligned |
| Temperature Drift | No | No |

MiBo Prototype

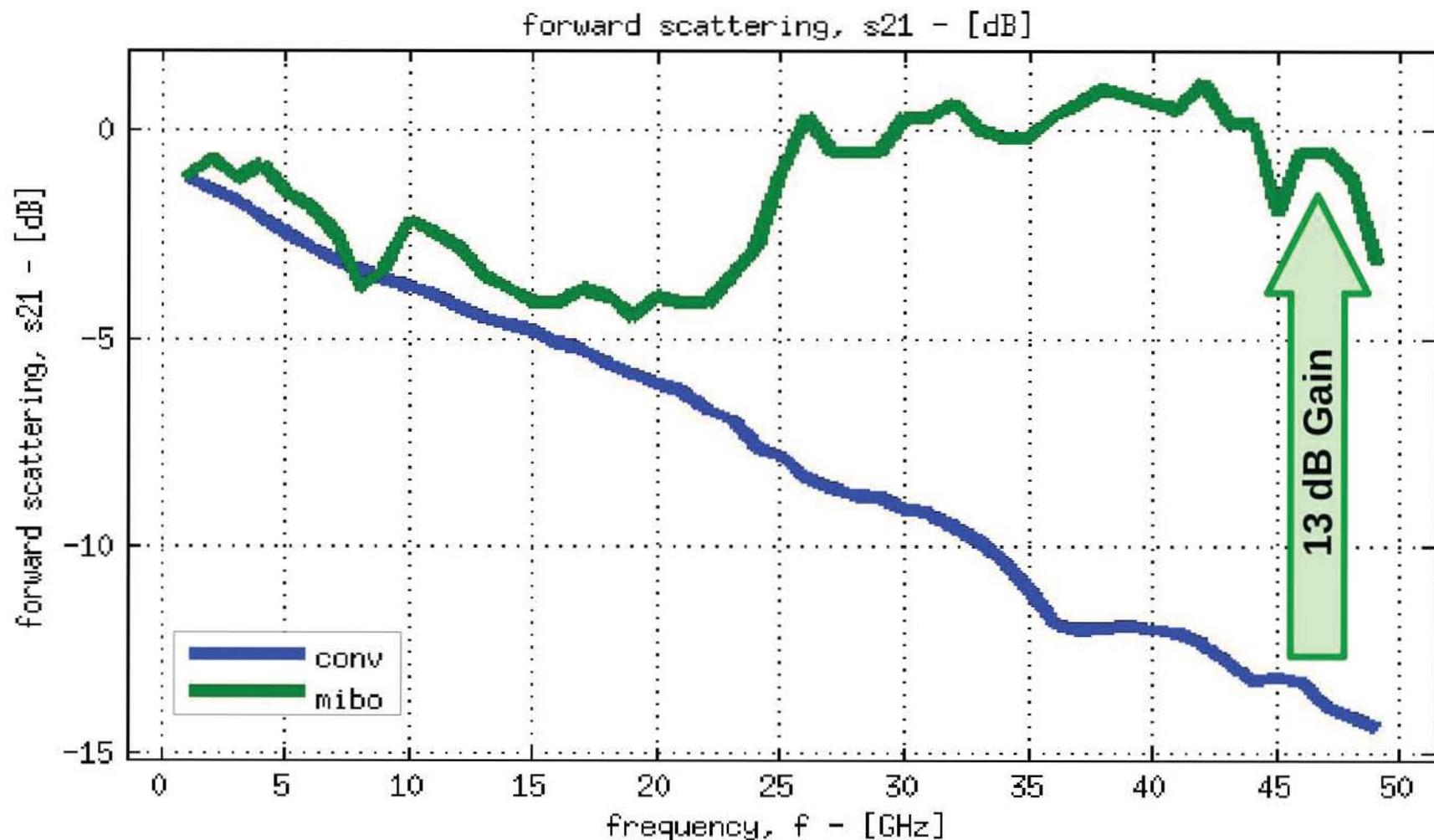
(Components Ordered and Received – Assembly underway)





Gen-2 MiBo Prototype -- Experimental Data

S₂₁ {MiBo; Conventional}

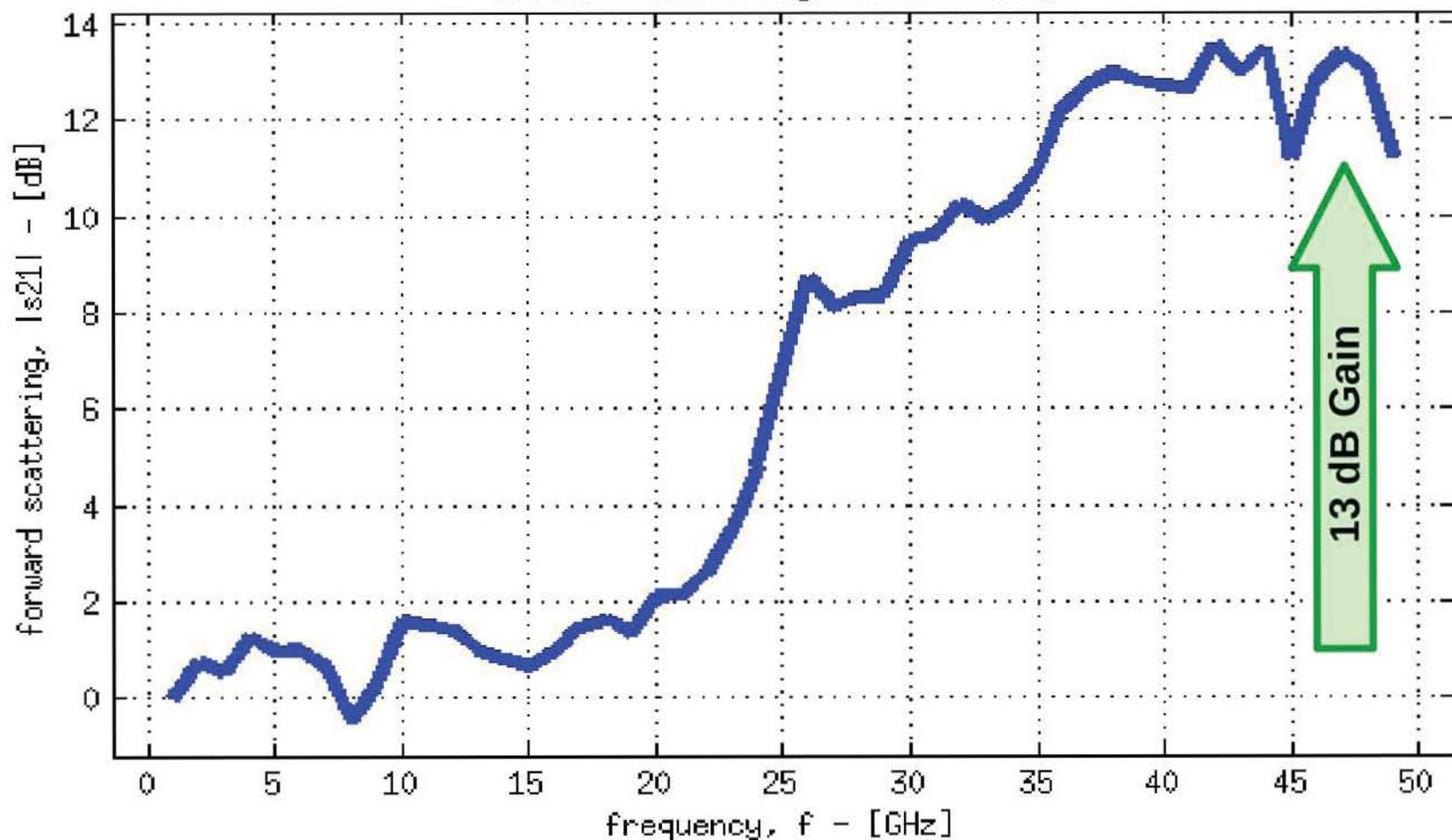


Gen-2 MiBo Prototype -- Experimental Data

MiBo Gain

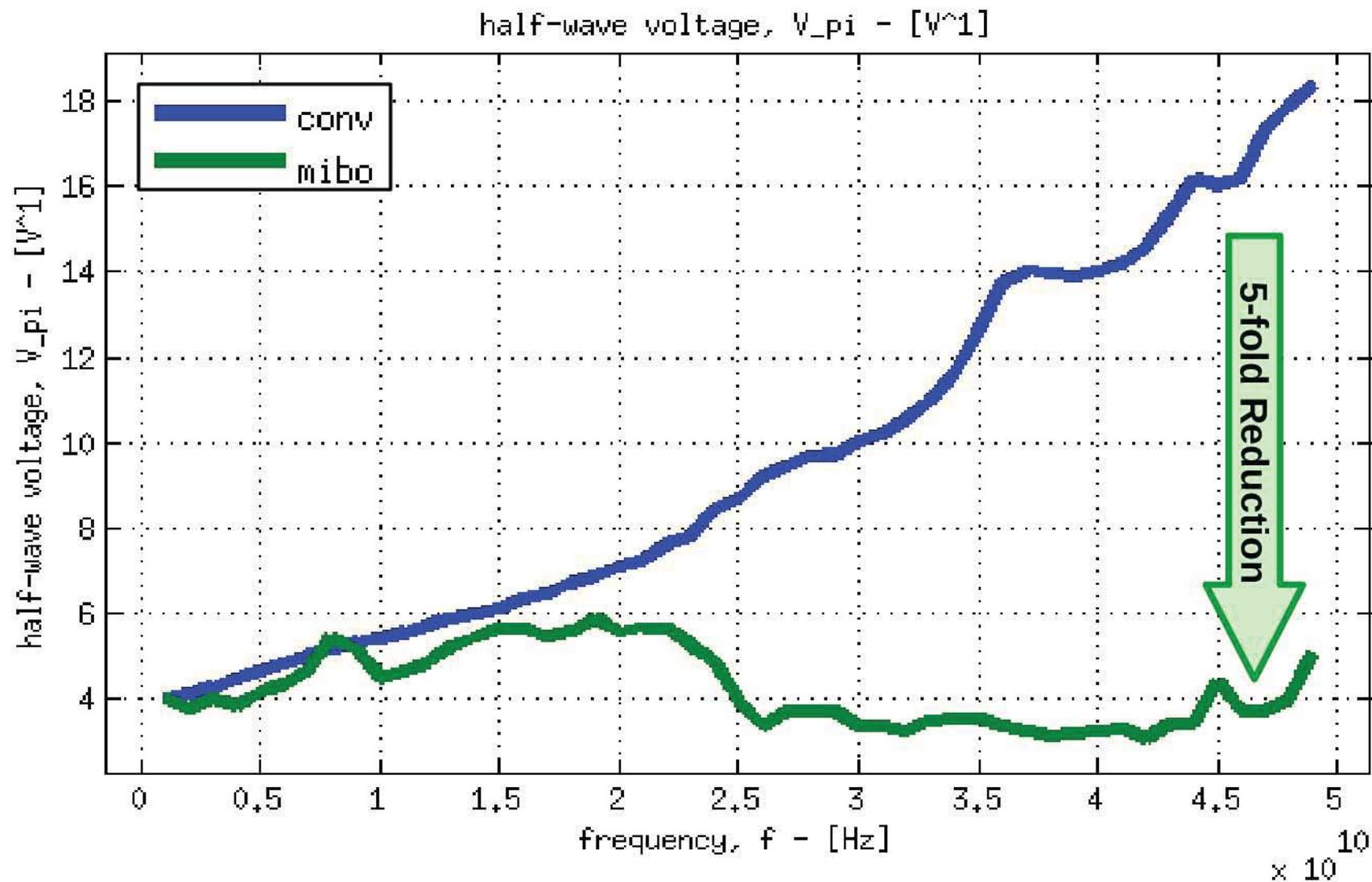


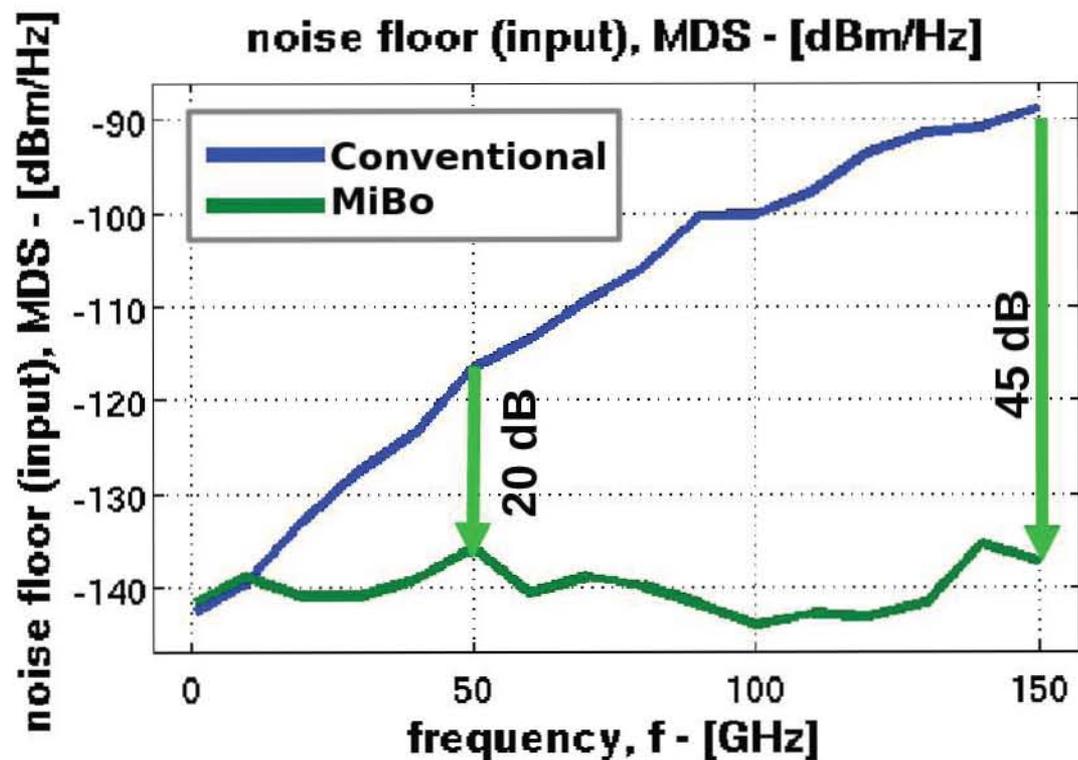
forward scattering, $|s_{21}|$ - [dB]



Gen-2 MiBo Prototype -- Experimental Data

Half-Wave Voltage





MiBo improves electrical Minimum Detectable Signal (MDS) by:
20 dB @ 50 GHz
45 dB @ 150 GHz

Simulations show MiBo can remotely sense signals as weak as -140 dBm/Hz from 1-150 GHz

Theoretical limit: -145 dBm/Hz Cox, IEEE Trans. MTT 2006, RIN=-175 dB/Hz.

Tracking an imploding cylinder with photonic Doppler velocimetry

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B. E. Blue,² and S. S. Walker³

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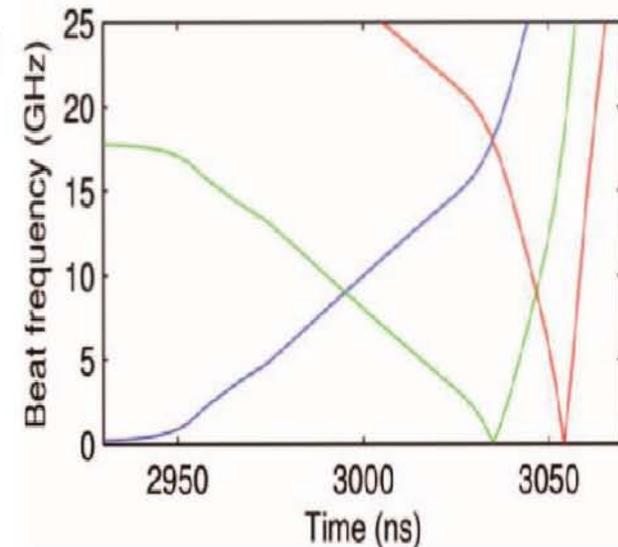
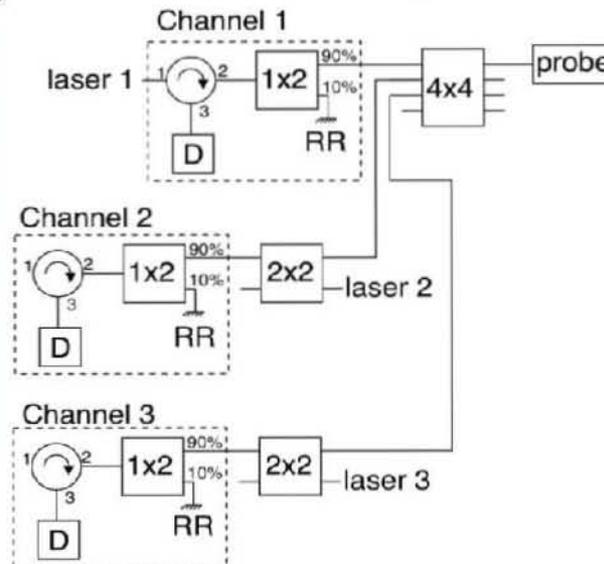
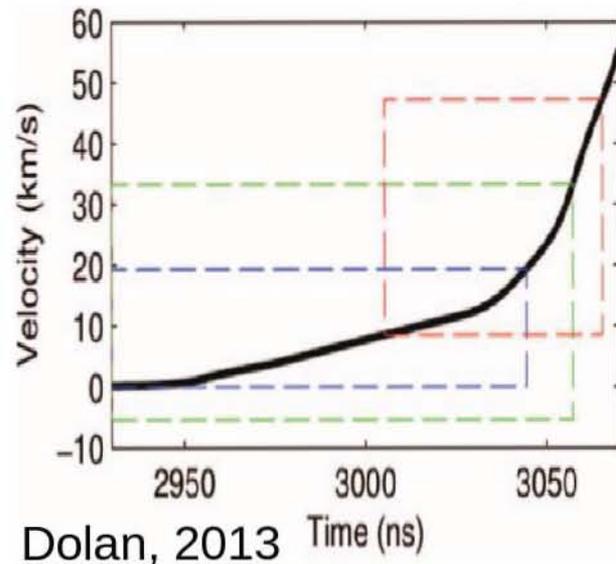
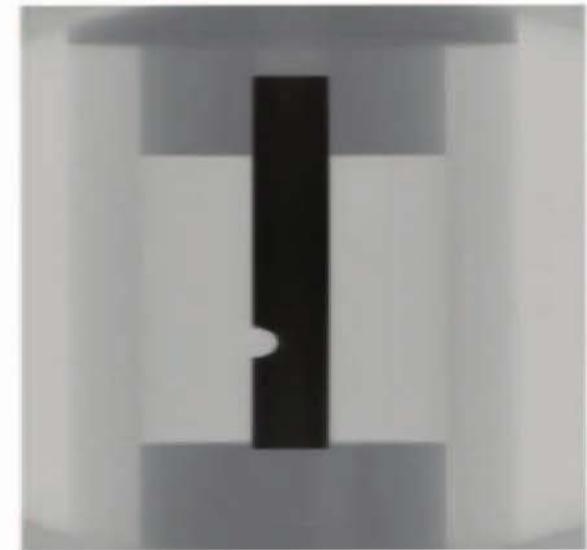
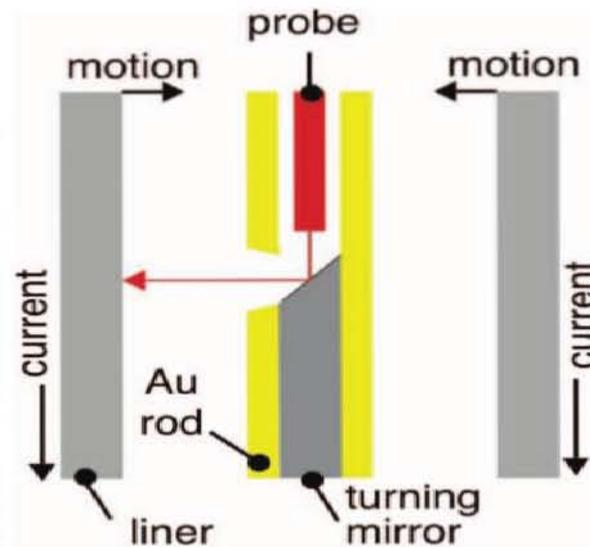
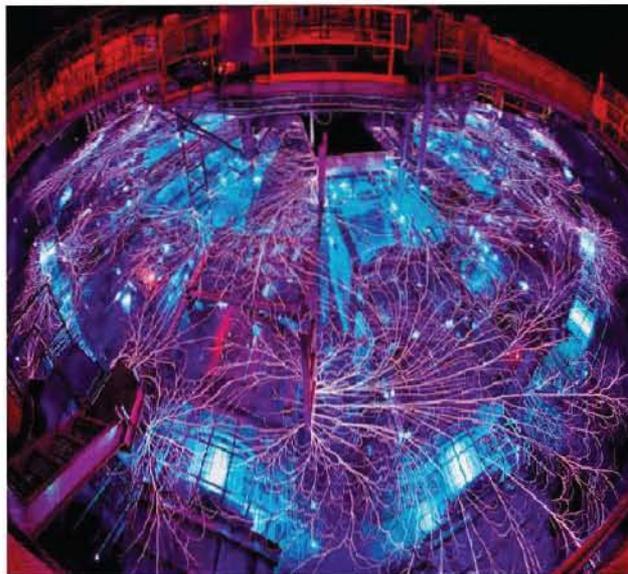
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(Received 1 March 2013; accepted 11 April 2013; published online 2 May 2013)

Cylindrical implosion offers a path to extreme material states, reaching considerably higher pressures than planar geometry. However, diagnosing compressed material in cylindrical geometry is challenging. Time-resolved velocimetry, a standard technique in planar compression, is difficult to incorporate into cylindrical experiments. This paper describes the use of photonic Doppler velocimetry (PDV) in magnetically driven cylindrical compression experiments at the Sandia Z machine. With this diagnostic, it is possible to track the interior of an imploding cylinder beyond 20 km/s. A “leapfrog” implementation is described to support velocities well above the bandwidth limits of standard PDV measurements. © 2013 AIP Publishing LLC. [<http://dx.doi.org/10.1063/1.4803074>]

PDV Example, Sandia Imploding Cylinder, 2013



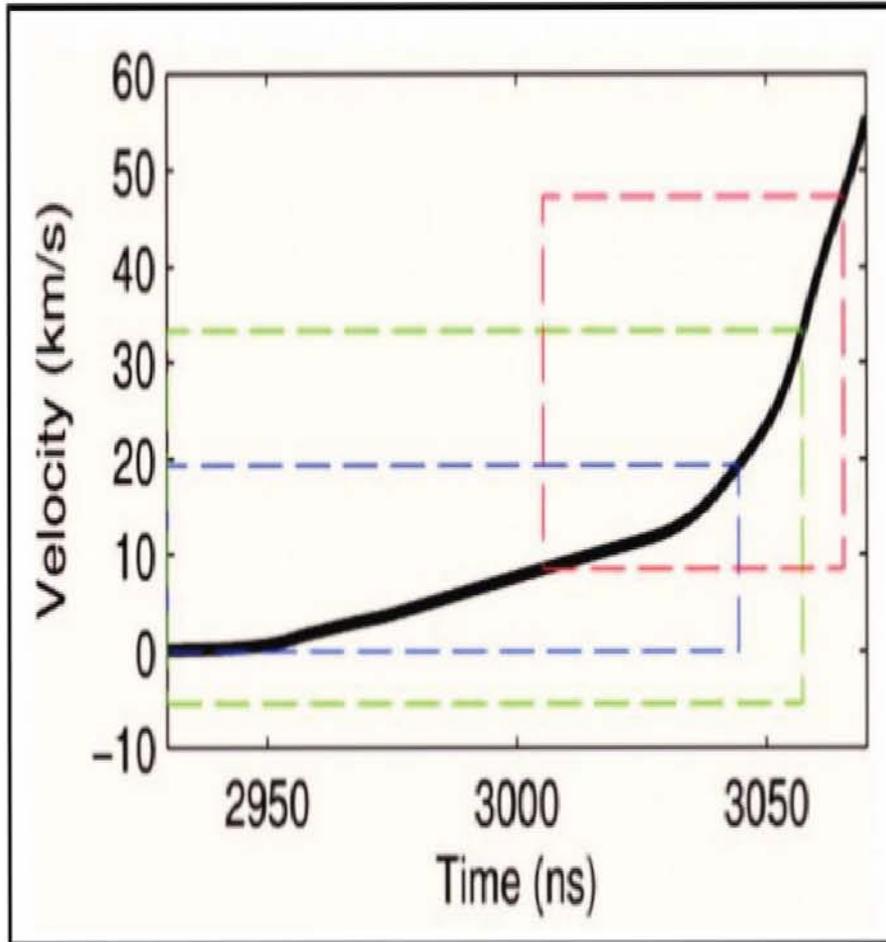


Figure 1: PDV data of Sandia target.¹

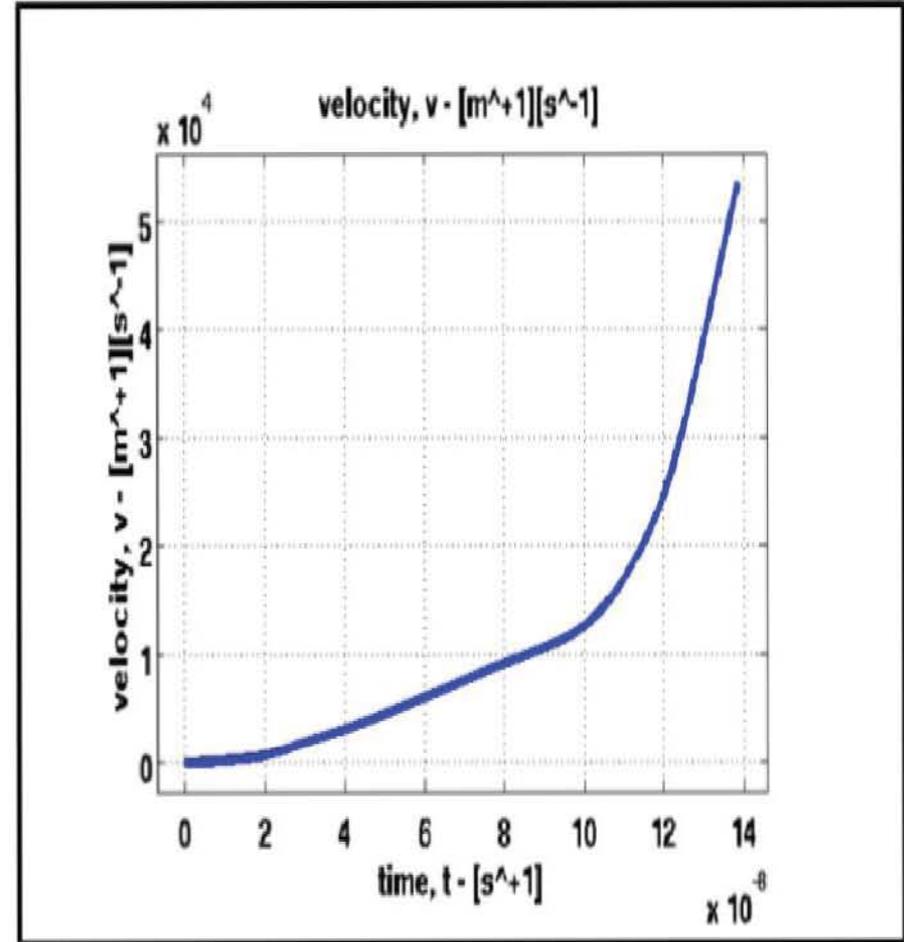


Figure 2: Digitized PDV data of Sandia target.

PDV Basics & Waveform Synthesis

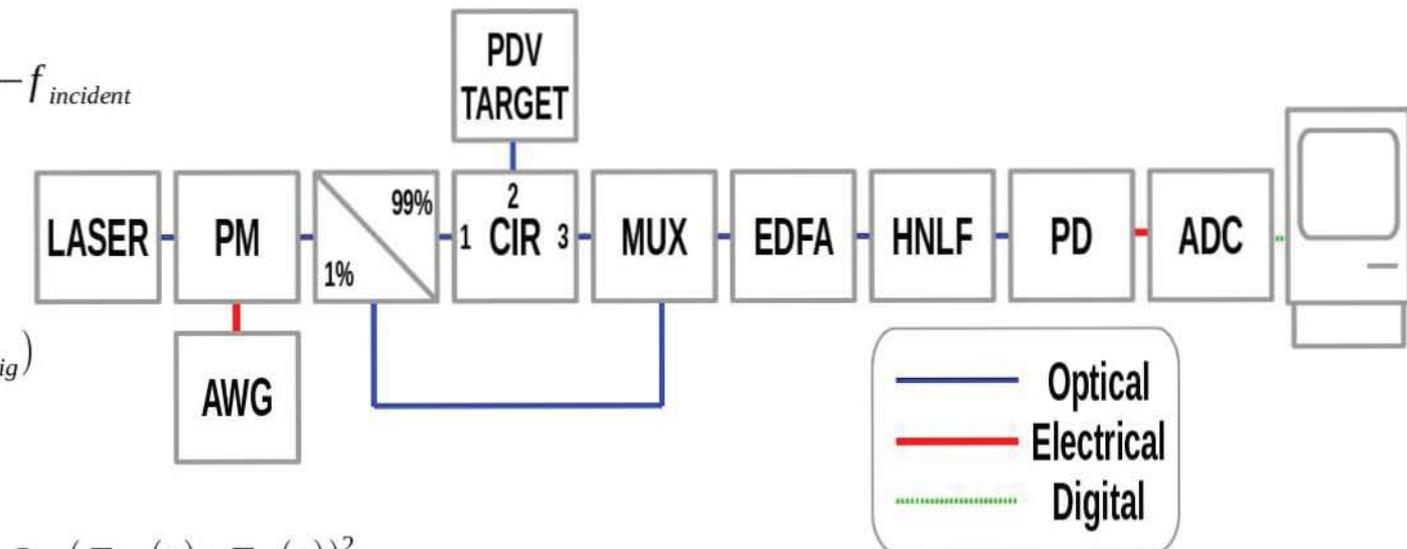


$$\Delta f = \frac{2\Delta v}{c} f_{incident} = f_{reflected} - f_{incident}$$

$$f_{reflected} = f_{incident} \left(1 + \frac{2\Delta v}{c}\right)$$

$$E_{sig}(t) = E_{sig} \cos(\omega_{sig} t + \phi_{sig})$$

$$E_{lo}(t) = E_{lo} \cos(\omega_{lo} t)$$



$$I \propto (E_{sig}(t) + E_{lo}(t))^2$$

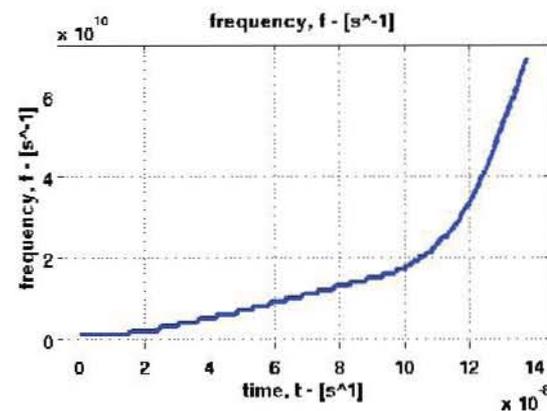
$$= (E_{sig} \cos(\omega_{sig} t + \phi_{sig}) + E_{lo} \cos(\omega_{lo} t))^2$$

$$= \frac{E_{sig}^2}{2} (1 + \cos(2\omega_{sig} t + 2\phi_{sig})) + \frac{E_{lo}^2}{2} (1 + \cos(2\omega_{lo} t))$$

$$+ E_{sig} E_{lo} [\cos((\omega_{sig} + \omega_{lo}) t + \phi_{sig}) + \cos((\omega_{sig} - \omega_{lo}) t + \phi_{sig})]$$

$$= \underbrace{\frac{E_{sig}^2 + E_{lo}^2}{2}}_{\text{constant component}} + \underbrace{E_{sig} E_{lo} \cos((\omega_{sig} - \omega_{lo}) t + \phi_{sig})}_{\text{beat component}}$$

$$\underbrace{+ \frac{E_{sig}^2}{2} \cos(2\omega_{sig} t + 2\phi_{sig}) + \frac{E_{lo}^2}{2} \cos(2\omega_{lo} t) + E_{sig} E_{lo} \cos((\omega_{sig} + \omega_{lo}) t + \phi_{sig})}_{\text{high-frequency component}}$$



Waveform Synthesis



$$I \propto \underbrace{\frac{E_{sig}^2 + E_{lo}^2}{2}}_{\text{constant component}} + \underbrace{E_{sig} E_{lo} \cos((\omega_{sig} - \omega_{lo})t + \phi_{sig})}_{\text{beat component}}$$

$$\omega_{sig} = \omega_{reflected} = \omega_{incident} \left(1 + \frac{2\Delta v}{c}\right)$$

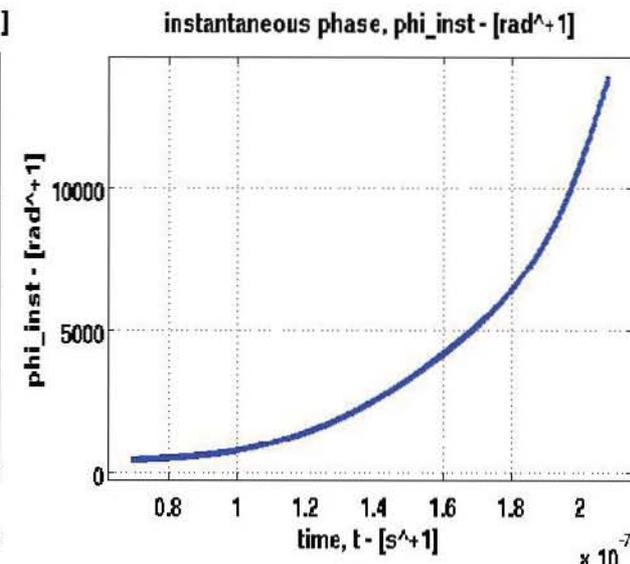
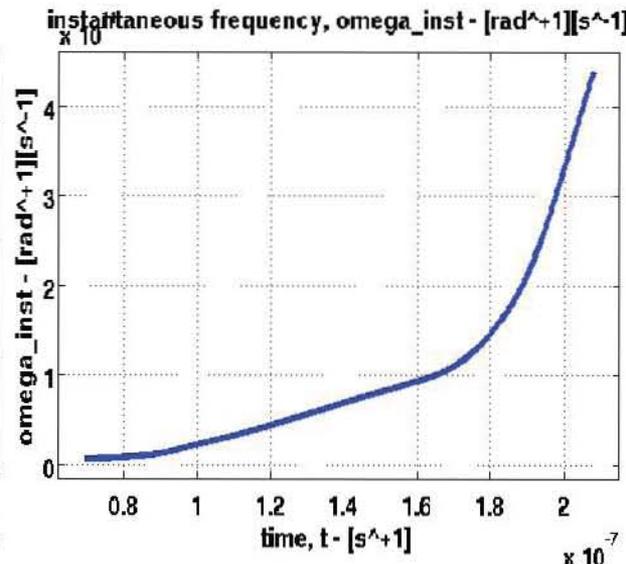
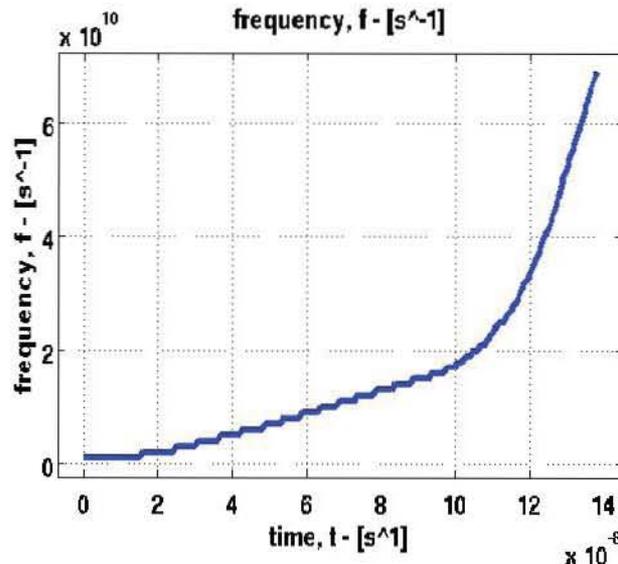
$$\Delta \omega_{offset} = \omega_{incident} - \omega_{lo}$$

$$P(t) = \frac{P_{sig} + P_{lo}}{2} + \sqrt{P_{sig} P_{lo}} \cos\left(\underbrace{\left(\frac{(\omega_{lo} + \Delta \omega_{offset})2\Delta v}{c} + \Delta \omega_{offset}\right)t + \phi_{sig}}_{\omega_{inst}(t)}\right)$$

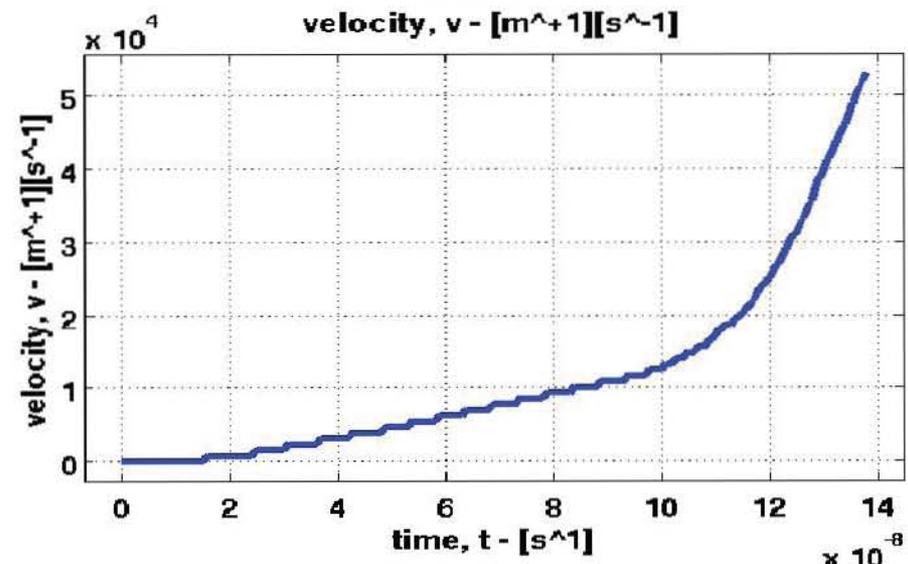
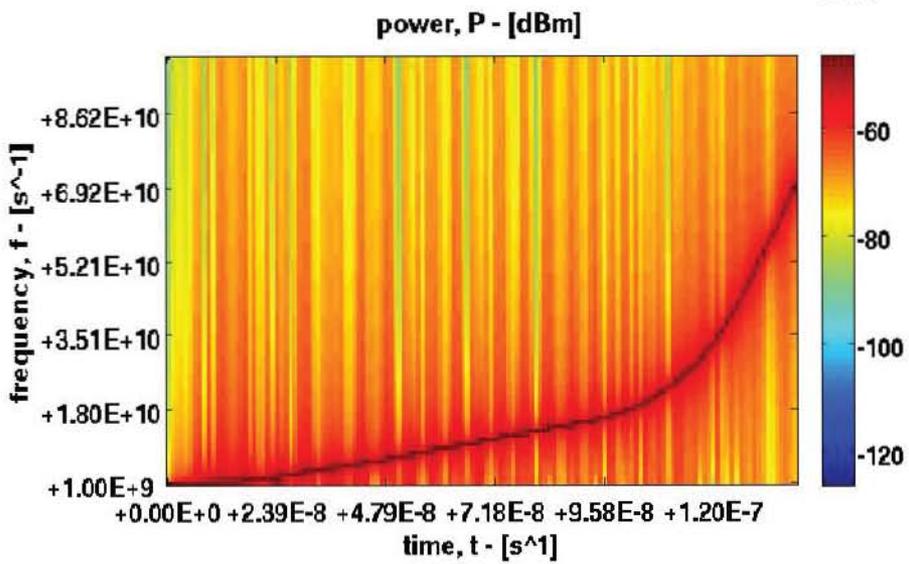
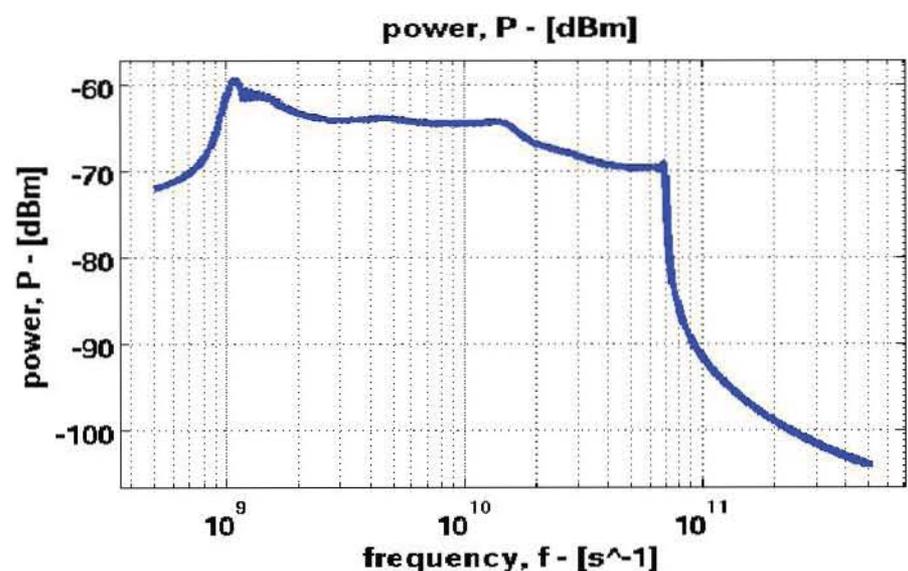
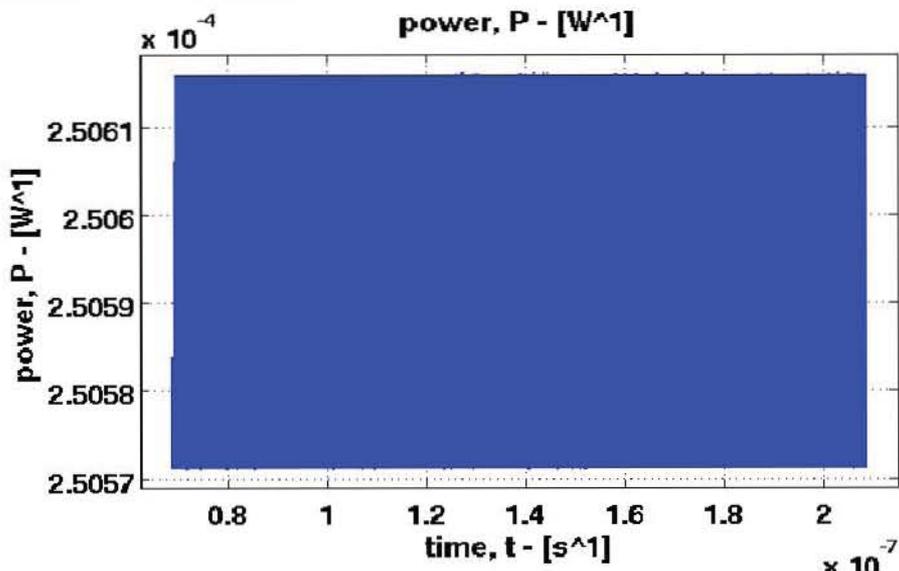
$$\omega_{inst}(t) = \frac{(\omega_{lo} + \Delta \omega_{offset})2\Delta v}{c} + \Delta \omega_{offset}$$

$$\phi_{inst}(t) = \int_{-\infty}^t \omega_{inst}(t') dt'$$

$$P(t) = \frac{P_{sig} + P_{lo}}{2} + \sqrt{P_{sig} P_{lo}} \cos(\phi_{inst}(t))$$



Waveform Synthesis



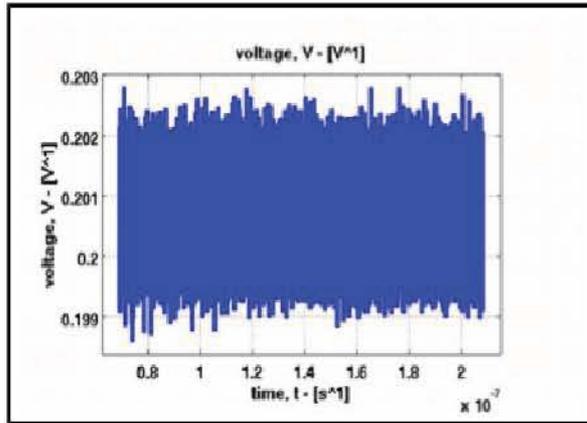


Figure 13: PD waveform.

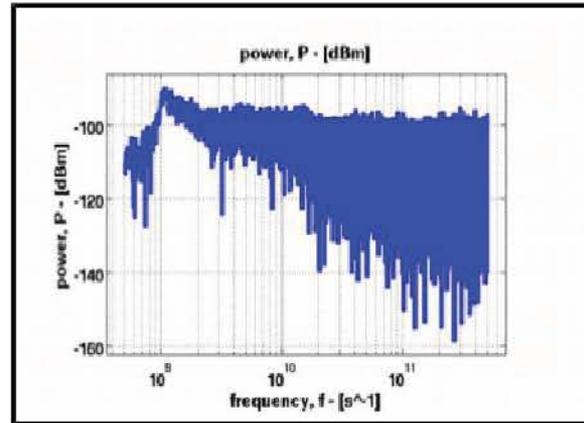


Figure 14: PD spectrum.

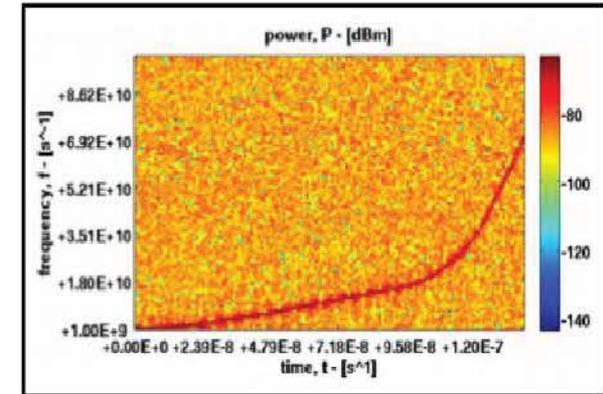


Figure 15: STFT of PD waveform.

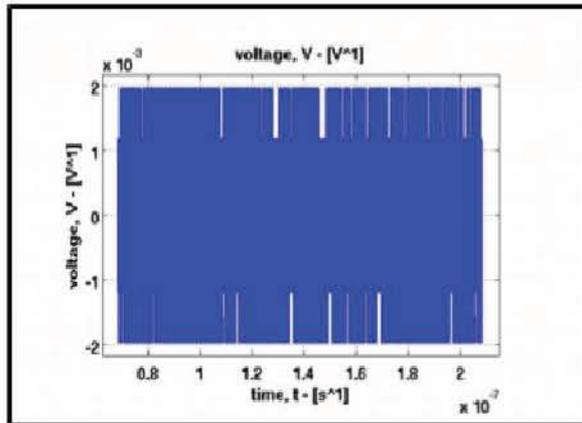


Figure 16: Digitized waveform

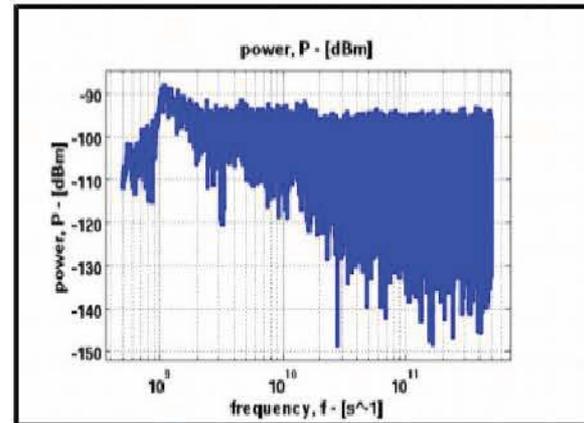


Figure 17: Digitized Spectrum

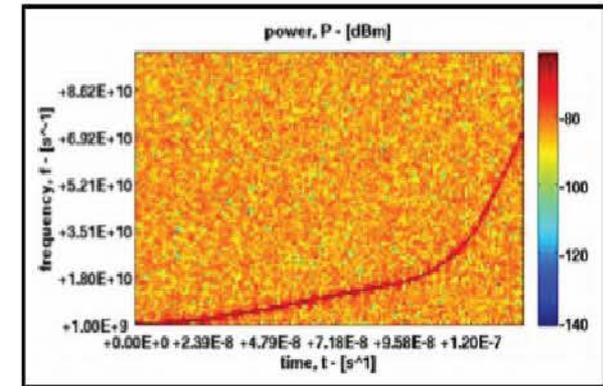


Figure 18: STFT of Digitized waveform.

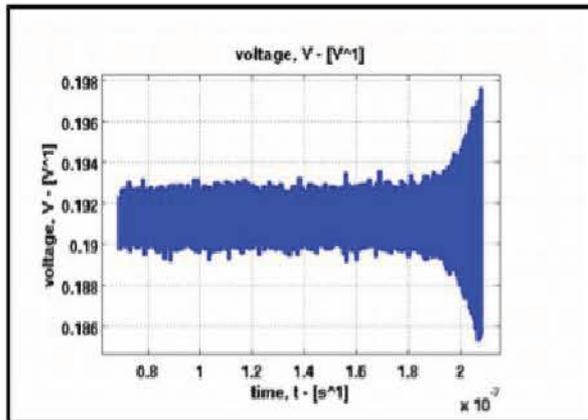


Figure 22: PD waveform.

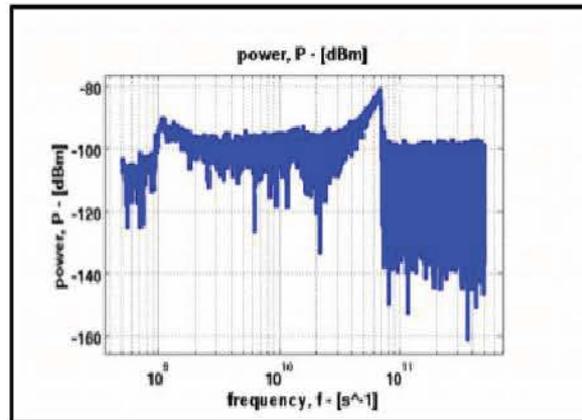


Figure 23: PD spectrum.

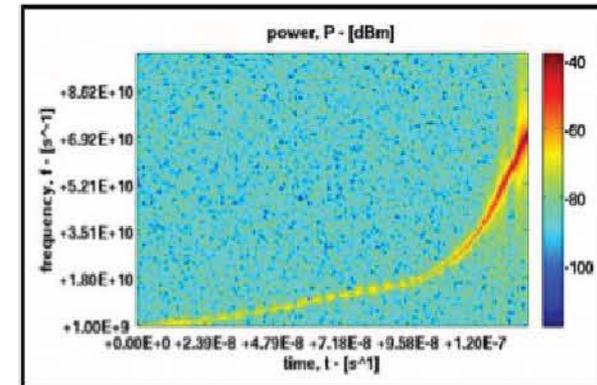


Figure 24: STFT of PD waveform.

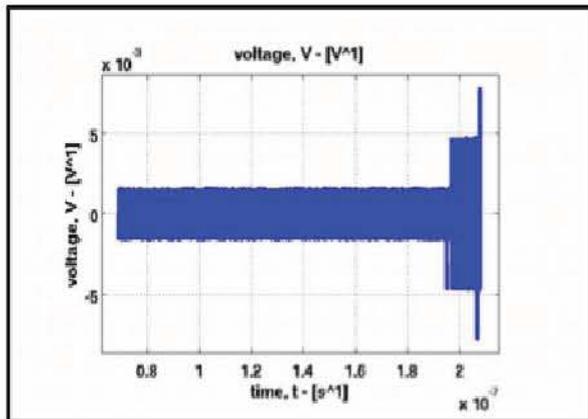


Figure 25: Digitized waveform

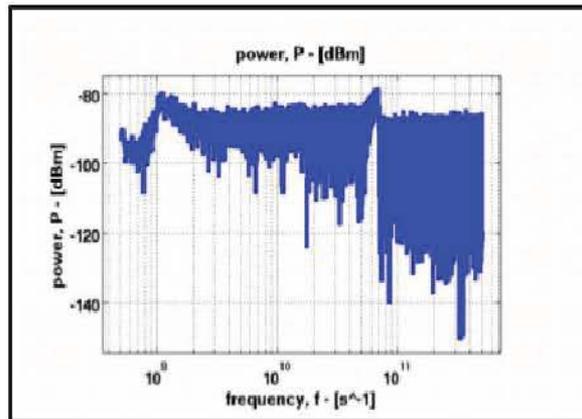


Figure 26: Digitized Spectrum

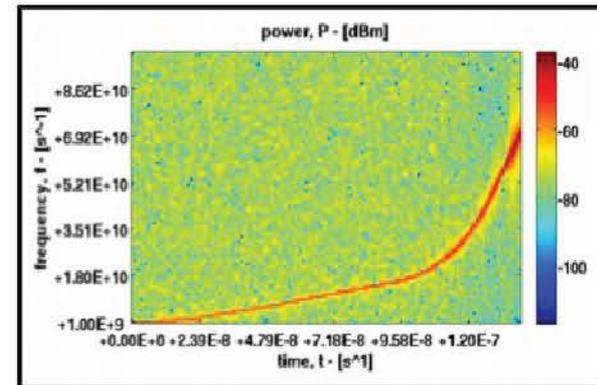
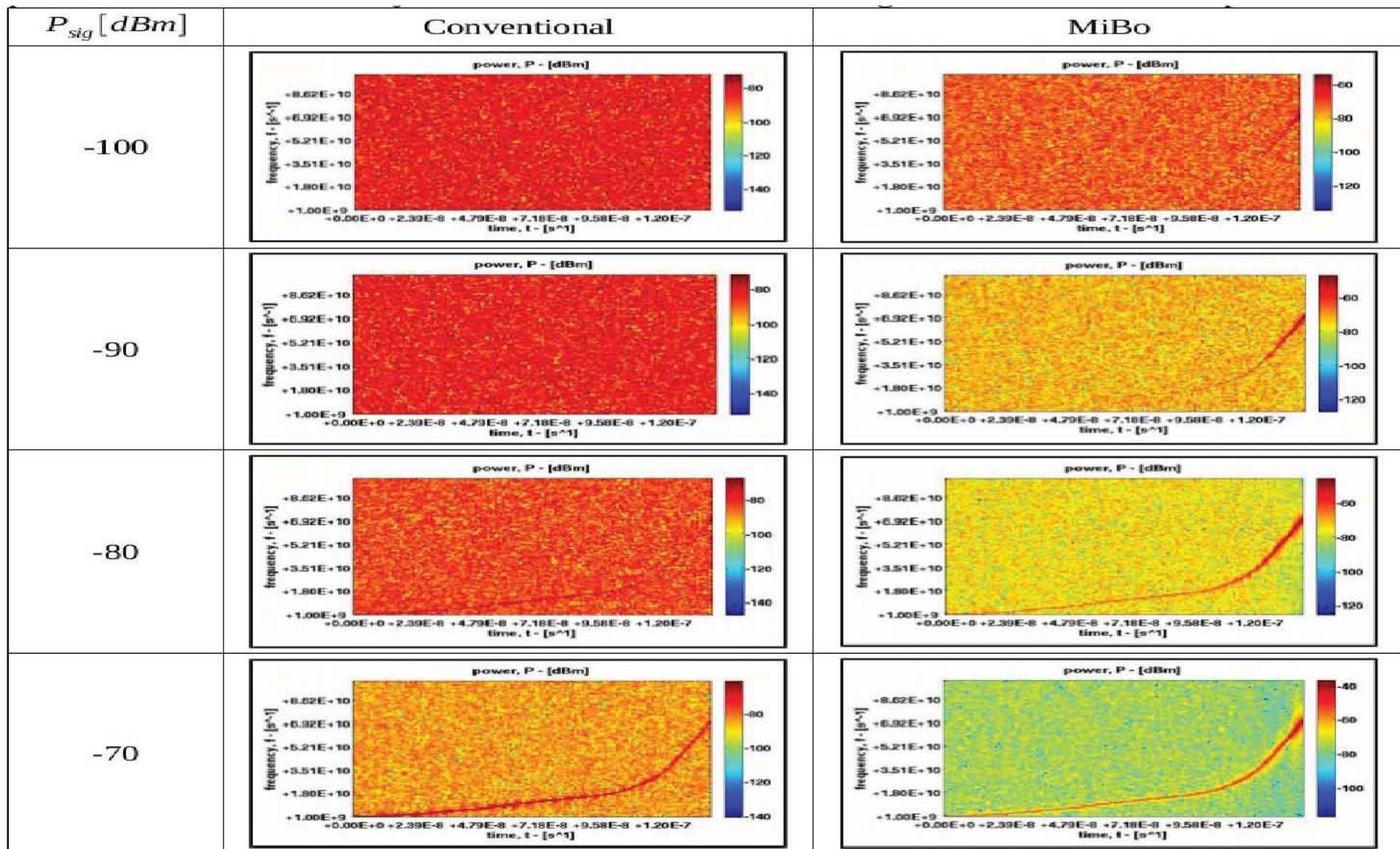


Figure 27: STFT of Digitized waveform.

Comparison



2015-09-03T10:24:16

201509031014-pdv-mibo-study

Photon Doppler Velocimetry & Modulation Index Boosting

A Proof-of-Principle Study

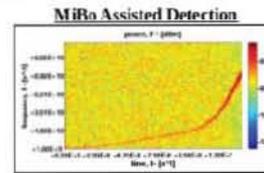
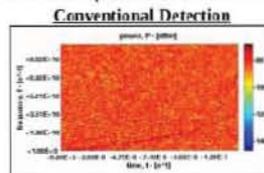
David Borlaug, Bill Seng, Crystal Glen, and Bahram Jalali

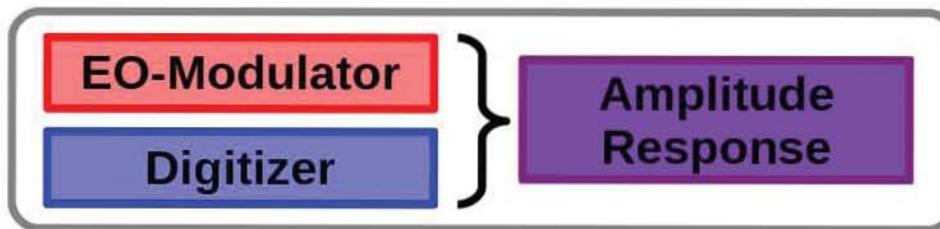
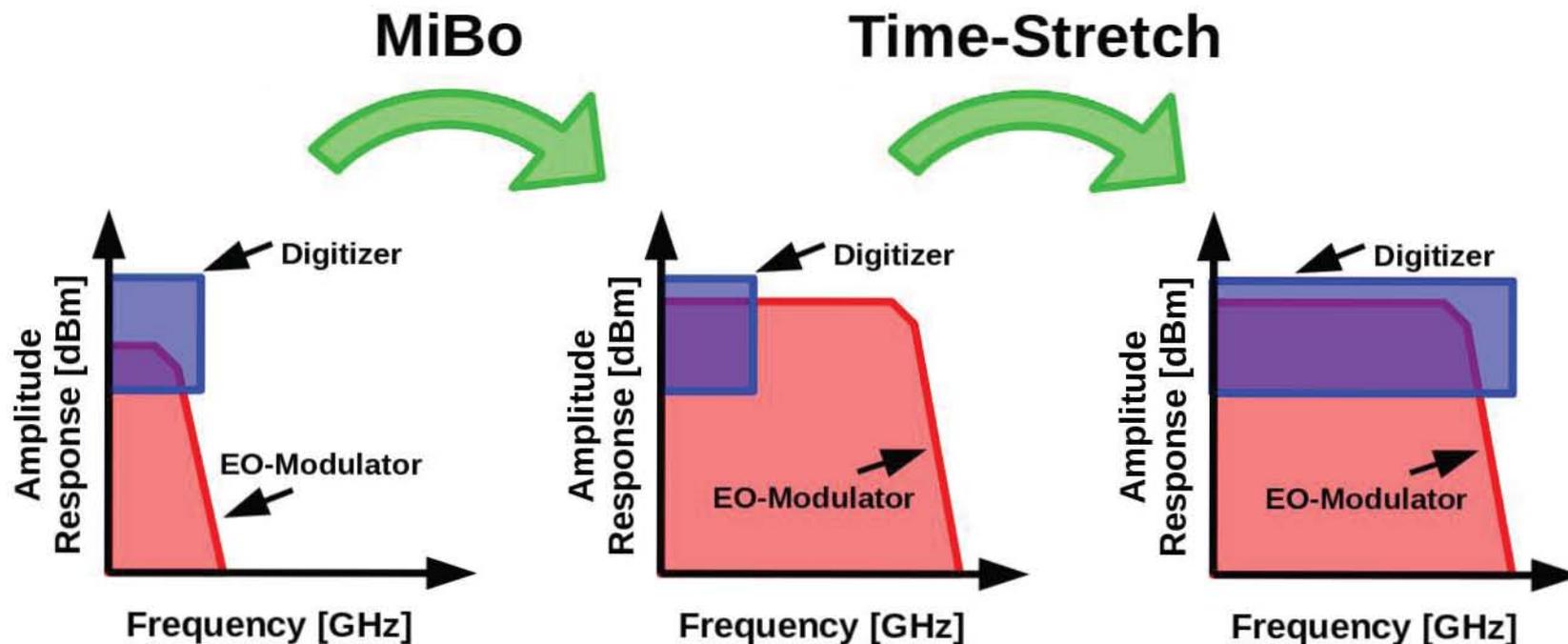
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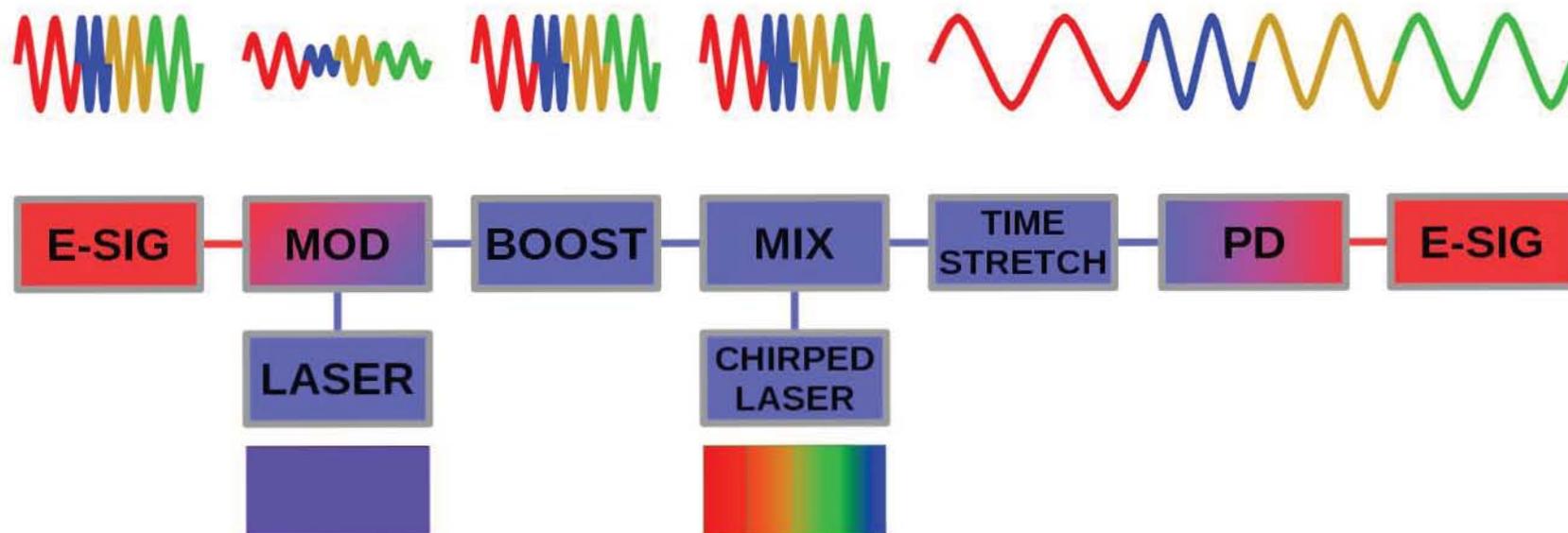
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| PDV Waveform Generation..... | 2 |
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| MiBo Assisted Detection..... | 8 |
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Executive Summary

The purpose of this study is to investigate the potential for performance enhancement by combining two mature techniques, Photon Doppler Velocimetry (PDV), developed by Sandia, and Modulation Index Boosting (MiBo), developed at UCLA in collaboration with Sandia. PDV utilizes Doppler velocimetry to track unconventionally high velocity objects. In the course of operation, PDV generates high-frequency broadband waveforms with spectral content from 1-70 GHz. MiBo is a technique that preferentially boosts or amplifies high-frequency signals by as much as 15 dB at 50 GHz. MiBo gain extends up to 150 GHz, making the technique especially relevant to PDV. This proof-of-principle study analyzes the expected performance impact of inserting a MiBo module in to a PDV system. The unoptimized results presented here show that MiBo is able to improve PDV detection sensitivity by 10 dB in general, and by as much as 20 dB for challenging Doppler frequency shifts beyond 40 GHz. These results offer a compelling case for further development of MiBo assisted PDV systems.







- MiBo has a high pass gain profile into the 100s of GHz -- can boost signals to overcome the information bottleneck.
- MiBo delivers 15 dB electrical signal power gain at 50 GHz.
- MiBo increases signal detectivity by 15 dB at 50 GHz.
- Time-Stretch MiBo enables high-sensitivity broad-band digitization using fair-sensitivity narrow-band digitizers.
- PDV can utilize MiBo in all-optical and electro-optical systems to capture fast moving velocimetry data.

Thank You
